

5                   METHOD AND APPARATUS FOR CONTROLLING A MOVING WEB

                  BACKGROUND OF THE INVENTION

10                   The present invention generally relates to a method and an apparatus for controlling a moving web. More specifically, the present invention relates to a web guide apparatus having minimal mechanical backlash cooperating with a high speed control system which allows for precise control of a transverse location of the moving web. The present invention further includes a method of controlling the transverse location of the web.

15                   Generally, there are two types of guide systems for controlling a transverse position of a moving web. A first type of guide system for controlling a transverse position of a moving web is a passive system.

20                   An example of a passive system is a crowned roller, also called a convex roller, having a greater radius in the center than at the edges. Crowned rollers are effective at controlling webs that are relatively thick in relation to the width of the web such as sanding belts and conveyor belts.

25                   Another passive type of guide system is a tapered roller with a flange. The taper on the roller directs the web towards the flange. The web edge contacts the flange and thereby controls the transverse position of the web. A tapered roller with a flange is commonly used to control the lateral position of a narrow web, such as a videotape.

30                   However, a passive guide system cannot guide wide, thin webs because, depending on the type of passive guide system, either the edge of the web tends to buckle or the web tends to develop wrinkles. To effectively control a wide, thin web an active guide system is required.

35                   A typical active guide system includes a sensing device for locating the position of the web, a mechanical positioning device, a control system for determining an error from a desired transverse location and an actuator that receives a signal from the control

system and manipulates the mechanical positioning device. A typical control system used for actively guiding a thin, wide web is a closed loop feedback control system.

Typically, a web to be processed has been previously wound onto a spool.

During the winding process, the web is not perfectly wound and typically has transverse positioning errors in the form of a zigzag or a weave. When the web is unwound, the zigzag or weave errors recur causing transverse web positioning problems.

In precision web applications such as webs used in optics and electronics, the transverse location of the web must be precisely controlled. Most commercially available active web guide systems are not capable of controlling the transverse location to the level of precision required for these web applications. Commercial web guides typically employ rod ends, belts, sheaves, slides and threaded nuts and bolts, each of which has some mechanical play. Often, in a commercially available guide, the total mechanical play is in range of 125-375 microns (0.005-0.015 inches). A control system cannot guide a web to within a range of the guide's backlash or mechanical play.

While the control system of a commercially available web guide has some error, often the error caused by the control system is insignificant when compared to the error caused by the mechanical backlash or play in the guide. The mechanical backlash, without accounting for any other error can preclude many commercially available web guides from being used for precisely locating a transverse location of a moving web.

#### BRIEF SUMMARY OF THE INVENTION

The present invention includes a method of controlling a moving web in relation to a selected transverse position comprising positioning a first positioning guide proximate a second positioning guide wherein the second positioning guide includes a mechanism for positioning the web having minimal backlash. The web is passed through the first positioning guide and the second positioning guide. A sensor detects the transverse position of the moving web at the second positioning guide. The sensor transmits the transverse location of the web at the second positioning guide to a controller. The controller manipulates a zero-backlash actuator where the zero-backlash actuator is coupled to the

second positioning guide such that the transverse position of the web is controllable to within a preselected dimension of the selected transverse position.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a schematic view of the precision web guide assembly of the present invention.

Figure 2 is a perspective view of a precision web guide of the present invention.

Figure 3 is an additional perspective view of the precision web guide of the present invention.

Figure 4 is an additional perspective view of the precision web guide of the present invention.

Figure 5 is an additional perspective view of the precision web guide of the present invention.

#### DETAILED DESCRIPTION

The present invention generally relates to an assembly for controlling a transverse location of a moving web. The assembly includes a first web guide in series with a second web guide. The first web guide is manipulated by a first control system and the second web guide is manipulated by a second control system. The first and second control systems control the first and second web guides independent of each other to provide precision control of the transverse position of the moving web.

The assembly provides precise control of the transverse position of the moving web because of a number of design features including, but not limited to, positioning the first web guide, having a short exit span, and upstream and proximate the second web guide. The first web guide reduces the input angle error, the transverse position error, and the error rate of the moving web entering the second web guide.

With the input angle error, the transverse position error, and the error rate reduced by the first web guide, the second web guide precisely controls the transverse position of the moving web. The second web guide is designed to be lightweight and stiff while minimizing backlash caused by mechanical play. The lightweight, stiff second web guide with minimal

backlash allows the second control system, having a fast, high resolution sensor communicating with a fast control system, to precisely control the transverse location of the moving web with a high bandwidth, zero backlash actuator connected to the second web guide with a zero backlash connection.

5 The second web guide also includes a relatively long guide span and a relatively short exit span. The long guide span reduces an angle needed to produce a correction to the transverse position of the moving web and reduces a twist angle of the moving web in the entrance and exit spans. The short exit span reduces the transverse position error caused by the input angle error.

10 As used herein, the terms “precision control” or “precise control” means controlling a transverse position of the web to within less than about 0.004 inches (0.0102 mm) of a desired location.

15 As used herein, the term “backlash” corresponds to the amount of mechanical play or lost motion found in the web guide. Backlash adversely affects the ability of a control system to precisely control the transverse position of the moving web.

As used herein, the term “zero-backlash” means tolerances or mechanical play of less than about 0.0001 inch (0.0025 mm).

20 As used herein, the term “exit span” means the distance between the last frame roller and the second base roller of the web guide that is preferably expressed in terms of a factor of a width of the web.

As used herein, the term “entrance span” means the distance between the first base roller and the first frame roller of the web guide that is preferably expressed in terms of a factor of a width of the web.

25 As used herein, the term “guide span” means the distance between the entrance span and the exit span. The guide span is preferably expressed in terms of a factor of a width of the web.

As used herein, the term “input angle error” is the error in the angular position of the web from the desired angle of the web as the web is detected by the sensor. Typically, the input angle error of the moving web is undetectable by a single web position sensor. Since a

web position sensor detects the position of the web at only one point, the sensor detects the position of the web, but not the input angle of the web. Therefore, a single sensor may detect no positional error while there may be a significant amount of input angle error that is undetected. The input angle error, although undetected by a single position sensor, may result in a significant downstream position error.

The present invention generally includes an assembly 10 and method for precisely controlling a transverse position of a moving web 12 as illustrated in Figure 1. The moving web 12 is passed through a first web guide 14 followed by a second web guide 16. While an exact distance between the first web guide 14 and second web guide 16 is not critical to practice the invention, it is preferred that first web guide 14 and second web guide 16 be disposed in close proximity with minimal or no intermediate processing of the web 12. In an exemplary embodiment, an idler roller 18 is disposed within the path of the moving web 12 between the first web guide 14 and the second web guide 16.

The first web guide 14 can include any conventional commercially available web guide. It is preferred that an exit span 20 between the last roller 21 and the second to the last roller 19 of the first web guide 14 be relatively short compared to an exit span of a conventional web guide. A short exit span 20 on the first web guide 14 significantly reduces the transverse angular error of the moving web 12, reduces the input angle error, and minimizes output error. The exit span 20 of the first web guide 14 is preferably less than about one-half of the width of the moving web 12. Upon reading this specification, one skilled in the art will appreciate that the shortest exit span possible is preferred that does not result in the wrinkling of the moving web 12. An exemplary commercially available web guide that can be used as the first web guide is a DF Rotating Frame Guide “P-Model” manufactured by BST Pro Mark of Elmhurst, Illinois.

Preferably, the first web guide 14 includes a first control system 22 that independently controls the first web guide 14. The first control system 22 is preferably a closed loop feed back system, although a feed forward system, H infinity system, model based system, embedded model based system or any other control system which will effectively control the transverse position of the moving web 12 is also within the scope of the invention.

The first control system 22 includes a first web position sensor 24 that preferably detects a position of an edge of the moving web 12. One skilled in the art will recognize that other position detecting sensors besides edge position sensors are within the scope of the invention. The first web position sensor 24 communicates with a first controller 26. The first controller 26 detects the error of the transverse position of the edge of the moving web 12 from a selected setpoint. The first controller 26 preferably employs a proportional-integral controller (PI) control scheme.

The first controller 26 communicates the error to an actuator 28. The actuator 28 adjusts the position of the first web guide 14 depending on the magnitude of error calculated by the first controller 26.

Referring to Figure 1, after the moving web 12 exits the first web guide 14, the moving web 12 preferably passes over the idler roller 18 prior to entering into the second web guide 16. After passing through the first web guide 14, the input error rate, the input angle error and the output transverse error of the moving web 12 have been significantly reduced as the moving web 12 enters the second web guide 16. The second web guide 16, as illustrated in Figures 2-5, is also referred to as a precision web guide. The precision web guide 16 manipulates the transverse position of the moving web 12 to within less than about 0.004 inches (0.102 mm) of a desired transverse location.

The moving web 12 passes over a first base roller 32 disposed within a base 30 of the precision web guide 16. The base 30 is fixed in a selected position, preferably with a plurality of bolts, however the base may be fixed into the selected position by a weld, a plurality of rivets or any other fastening means which fixedly retains the base in the selected position.

The base 30 also includes a second base roller 34 disposed therein. Preferably, an axis 35 of the first base roller 32 is substantially parallel to an axis 37 of the second base roller 34. Both the first and second base rollers 32, 34, respectively, include laterally loaded or precision bearings. The laterally loaded or precision bearings are preferred to minimize or eliminate lateral backlash within the first and second base rollers 32, 34 respectively. An exemplary laterally loaded bearing can be purchased along with an Ultralight Aluminum Idler manufactured by Webex, Inc. of Neenah, Wisconsin.

After passing over the first base roller 32, the moving web 12 contacts and passes over a first frame roller 38 that is disposed within a frame 36. The frame 36 is connected to the base 30 but is also movable with respect to the base 30. Preferably, the frame 36 is connected to the base 30 with a plurality of flexure plates 40, 42, 44, 46 as viewed in Figures 1-5. The plurality of flexure plates 40, 42, 44, 46 allows the frame 36 to move relative to the base 30 without any mechanical backlash or mechanical play. Although a plurality of flexure plates 40, 42, 44, 46 is preferred, one skilled in the art will recognize that other connecting mechanisms which allow the frame to move relative to the base with minimal or no mechanical backlash are within the scope of the invention. The alternative connecting mechanisms include, but are not limited to, linear ways, a precision pivot, and preloaded mechanical components.

Referring to Figures 2-5, a length of each flexure plate 40, 42, 44, 46 is significantly longer when compared to a width of each flexure plate 40, 42, 44, 46. The flexure plates 40, 42, 44, 46 are designed to flex along the width of the flexure plate while maintaining stiffness along the length of the plate. In the exemplary embodiment, the frame is connected to the base with four flexure plates 40, 42, 44, 46.

The four flexure plates 40, 42, 44, 46 connect the frame 36 to the base 30 such that the frame 36 rotates about a point 48 proximate the first frame roller 38. Referring to Figures 2 and 3, an optional pivot pin 49 is disposed between the frame 36 and the base 30 where the pivot pin 49 is fixed to the frame 36 but rotatable with respect to the base 30. The pivot pin 49 is disposed within a bracket 51 attached to the base 30 to retain the pivot pin 49 in the selected position while allowing the pivot pin 49 to rotate therein.

Referring to Figures 2-5, the first and second flexure plates 40, 46, respectively, attach the frame 36 to the base 30 proximate ends 39 of the first frame roller 38. The first and second flexure plates 40, 46 are positioned such that the lengths of the flexure plates 40, 46 are substantially parallel to an axis of the first frame roller 38.

The third and fourth flexure plates 42, 44 connect the frame 36 to the base 30 between the first frame roller 38 and a second frame roller 50. The third and fourth flexure plates 42, 44, respectively are positioned at angles which are mirror images of each other as referenced

from a plane perpendicularly intersecting a midpoint of the first frame roller 38. While the first and second flexure plates 40, 46, respectively, allow the frame 36 to move forward and backward relative to the path of the moving web 12; the third and fourth flexure plates 42, 44, respectively, allow the frame 36 to twist or rotate relative to the path of the moving web 12.

5 The four flexure plates 40, 42, 44, 46 working in cooperation allow the frame 36 to pivot about the point 48 proximate the first frame roller 38. An exemplary pivot point 48 is about at the midpoint of an entrance tangent line of the moving web 12 with the first frame roller 38. In the context of this disclosure, what is meant by the entrance tangent line is the line defined by the first contact of the moving web with a roller.

10 After passing over the first frame roller 38, the moving web 12 passes over the second frame roller 50. The first and second frame rollers 38, 50, respectively, are also equipped with laterally loaded or precision bearings to minimize the amount of lateral backlash within the first and second frame rollers 38, 50. An exemplary laterally loaded bearing can be purchased along with an Ultralight Aluminum Idler manufactured by Webex, Inc. of Neenah, 15 Wisconsin.

One skilled in the art will recognize that one large roller may be substituted for the first and second frame rollers 38, 50, respectively. Additionally, one skilled in the art will recognize that the moving web 12 may pass over more than two rollers within the frame 36 while precisely controlling the transverse location of the moving web 12.

20 An axis 51 of the second frame roller 50 is approximately parallel to an axis 41 of the first frame roller 38. A distance from the first frame roller 38 to the second frame roller 50 defines a guide span 53 as best illustrated in Figure 1. The guide span 53 is relatively long as compared to the width of the moving web 12.

25 One skilled in the art will recognize that a longer guide span reduces the amount of movement required by the flexure plates 40, 42, 44, 46 to produce a desired transverse position correction. The ability to control the transverse position of the moving web 12 with a minimal amount of movement allows for a more accurate web guide control because twist angles in an entrance span 55 and an exit span 57 are minimized.

Additionally, minimizing the amount of movement while accurately controlling a transverse position of the moving web 12 allows use of the flexure plates 40, 42, 44, 46 that have no mechanical backlash, but also have a limited range of motion. If significant motion were required, the movement may exceed the flexibility of the flexure plates 40, 42, 44, 46, thereby precluding the use of flexure plates in the present invention.

After passing over the last frame roller 50, the moving web 12 passes over the second base roller 34. In an exemplary embodiment, the path of the moving web 12 in the entrance and exit spans 55, 57, respectively is substantially perpendicular to a plane of rotation of the frame 36. Applying the principles taught herein, one skilled in the art will appreciate that other web paths are within the scope of the invention, including but not limited to, the first base roller 32 being disposed above the first frame roller 38 and also at an angle not substantially perpendicular to the first frame roller 38. Similarly, the second base roller 34 may be disposed in a position such that the path of the moving web 12 is not substantially perpendicular to the plane of rotation of the frame 36.

Referring to Figure 1, a second control system 52 controls the precision web guide 16. The second control system 52 is preferably a closed loop feed back system. However, a feed forward system, H infinity system, model based system, embedded model based system or any other control system which will effectively control the transverse position of the moving web 12 is also within the scope of the invention.

The second control system 52 includes a second web position sensor 54 that detects a position of the edge of the moving web 12. One skilled in the art will recognize that other position detecting sensors besides edge position sensors are within the scope of the invention. The second positioning sensor 54 preferably includes a fast, high-resolution means of sensing a transverse position of the moving web 12 at an edge of the moving web 12 such as, at a minimum, a fifty-hertz sensor with at least twelve-micron resolution. A preferred second sensor 54 is a high speed, high precision digital micrometer Model No. LS-7030M manufactured by Keyence Corporation of America of Woodcliff Lake, New Jersey.

The second positioning sensor 54 preferable detects the transverse position of the moving web 12 at about or proximately below an exit tangent line 60 of the moving web 12

5 exiting the second frame roller 50. In the context of this disclosure, what is meant by the exit tangent line is the line defined by the last contact of the moving web with a roller. By sensing the transverse position at about or proximately below the exit tangent line 60 of the second frame roller 50, a transportation lag is minimized. What is meant by transportation lag is the transportation time from the last shifting roller, in this case the second frame roller 50, to the second positioning sensor 54.

10 However, the transverse position of the moving web 12 can be measured at numerous other locations including lower on the exit span or at about an exit tangent line of the moving web 12 exiting the second base roller 34. At these alternative transverse position sensing locations, the transportation lag will need to be accounted for in the control system.

15 The detected transverse position of the moving web 12 by the second web position sensor 54 is transmitted to a second controller 56. The second controller 56 compares the transverse position of the moving web 12 to a desired position or setpoint and calculates an error of the detected position from the desired position. The second controller 56 is typically a programmable logic controller using a proportional-integral (PI) controller with an update rate of at least about one millisecond. An exemplary controller is a TwinCAT PLC manufactured by Beckhoff Industrie Elektronik of Verl, Germany.

20 The second controller 56 communicates the error to a second actuator 58. The second actuator 58 is mounted to the base 30 or another stationary structure. Referring to Figures 2-5, the second actuator 58 is coupled to an extension 60 of the frame 36 that extends beyond the second frame roller 50 with a flexible bracket 62. The flexible bracket 62 is preferred to provide a zero backlash coupling of the actuator 58 to the frame 36. Further, the flexible bracket 62 allows the actuator 58 traveling in a linear motion to be coupled to the frame 36 that is traveling in an arcuate motion.

25 The plurality of flexure plates 40, 42, 44, 46 are designed to allow the frame 36 to rotate in a plane about the point 48 proximate the first frame roller 38 at about a midpoint of the entrance tangent line. As the frame 36 pivots about the point 48, an end 64 opposite the pivot point 48 moves in an arc. The flexible bracket 62 provides flexibility to allow the linear actuator 58 to cooperate with the frame 36 moving in an arcuate path.

The second actuator 58 has zero-backlash allowing for precise movement without mechanical play. The second actuator 58 is capable of control frequencies in excess of five hertz. An exemplary actuator is Model No. SR31-0605-XFM-XX1-238-PF-19413 manufactured by EXLAR ([www.exlar.com](http://www.exlar.com)). One skilled in the art will recognize that a direct linear or rotary motor may be used to practice the invention in place of the zero-backlash actuator.

The second actuator 58 does not require a significant amount of travel because the transverse position error is significantly reduced by the first web guide 14 and the first control system 22. Referring to Figures 4 and 5, a member 66 extending from the frame 36 towards the base 30 cooperates with first and second limit switches, 68, 70, respectively. If the member 66 contacts either of the limit switches 68, 70, the moving web 12 is stopped so that the web 12 can be manually realigned within the assembly 10.

The frame 36 is designed to have excess material removed to decrease the mass of the frame 36 while maintaining the required stiffness. Removing the excess material results in the frame 36 having a high natural frequency. Further, the decrease in mass of the frame 36 allows for a high system gain on the precision guide 16. The precision guide 16 of the present invention has a gain of greater than about thirty-three inverse seconds and a crossover frequency of greater than about five hertz.

Although the present invention has been described with reference to preferred embodiments, one having ordinary skill in the art will recognize that changes may be made in form and detail without departing from the spirit and scope of the invention.